

The 10^{-5} and $7.05 \times 10^{-4} \text{ cm}^2 \text{ s}$, also



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The group IV-VI transition metal carbides are harder and have the highest melting temperatures of all known compounds. This leads to their wide use in tooling, with the capability of operating in extreme conditions, even under significant loading. It is not, however, WC's superior hardness or refractory properties that make it a more suitable material for tooling than the other transition metal carbides. With a melting temperature of around 3060 K and a hardness between 18 and 22 GPa at room temperature, WC does not have the highest melting temperature or hardness when compared to the others [5–8].

It is a combination of WC's hardness over a range of temperatures, its high Young's modulus, which is twice that of the other carbides ($\sim 700 \text{ GPa}$) and its low thermal expansion coefficient, which is only half that of the other carbides ($\sim 5.5 \times 10^{-6} \text{ K}^{-1}$) [5, 15].

Diffusional Properties

When interpreting deformation at high temperature, it is important to know the coefficients of diffusion. Self-diffusion of ^{14}C in WC has been studied by C. P. Buhsmer and P. H. Crayton [16]. Data was collected at temperatures between 2238 and 2643 K. It was observed that there are two diffusion mechanisms, bulk and grain boundary diffusion. An anomalous volume diffusion coefficient was measured between 2.

5.6×10^{-15} (at 2238 K) and $5.88 \times 10^{-14} \text{ cm}^2/\text{s}$ (at 2643 K), increasing with temperature [16]. The grain-boundary diffusion coefficient was measured to be between 5.10×10^{-5} and $7.05 \times 10^{-4} \text{ cm}^2/\text{s}$, also increasing with temperature [16]. The activation energies for these processes were calculated to be around 368 kJ/mol for the bulk diffusion and between 297 and 310 kJ/mol for the grain boundary diffusion [16]. These values suggest that grain-

boundary diffusion will almost always dominate, which can be rationalised by considering the ratio of grain boundary diffusion to bulk diffusion, D_{GB}/D_{bulk} .

At a temperature of 1000 K this ratio is around 10^3 to 10^6 . We can therefore calculate at this temperature, the grain size at which grain boundary diffusion will dominate using the equation:
$$\frac{D_{GB}}{D_{bulk}} = \frac{f \delta}{d}$$
 where f is the volume fraction of grain boundaries, which can be calculated using a simple cuboidal grain shape to be approximately:
$$f = \frac{4\delta}{d}$$
 where δ is the width of the grain boundary and d is the average width of the grain. In the limit of large grain size, $(1-f) \approx 1$, therefore, the grain size at which the grain boundary diffusion will exceed bulk can be estimated as:
$$d_{crit} = \frac{4\delta}{1}$$
 Assuming a grain boundary width of 0.5 nm, d_{crit} is about 2 nm.

5 μm , i. e. at grain sizes below this, grain boundary diffusion should dominate, while at larger grain sizes, bulk will. This can then be compared to pure metals and pure oxides. Pure metals tend to have a value of 10^4 – 10^6 whilst pure oxides have a value close to 10^3 – 10^4 .

i. e., the d_{crit} of pure metals is typically 10 μm to 1 nm, while for oxides they are estimated to be in the nm range. The comparison of these ratios suggests that the diffusion characteristics of WC are an intermediate between pure oxides and pure metals. Deformation Mechanisms in

Ceramics When materials are used in high temperature applications, such as in a nuclear fusion reactor, creep can lead to significant deformation.

Creep is the sustained (time dependant) plastic strain resulting from an applied stress, usually seen at temperatures greater than $0.5 T_m$ [20]. There are three distinct stages of creep.

The first is primary creep, in which the strain rate begins high but decreases over time. The strain rate eventually comes to an equilibrium, leading to the secondary creep stage, steady-state creep. The third stage is tertiary creep, in which the strain rate increases up until failure. Tertiary creep is typically only seen when the material is in tension and is due to the formation of voids or onset of necking [20].

Although there are multiple mechanisms of creep in ceramics, many of these are not expected to operate in monolithic tungsten carbide (for example, viscous flow creep requires the presence of a liquid phase, and can therefore be excluded in this project). In practice, deformation of transition metal carbides tends to be dominated by three mechanisms (see Figure 2) [21]. Therefore, this section will focus primarily with these: low temperature plasticity, diffusional flow and power law creep. In addition, it will consider grain boundary sliding.