

# Power system security economy availability engineering essay

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Introduction quality are the main objectives. Last three of which, directly affect the customer. But in the recent years due to the rapid development in the electronics and digital computers the nature of the load has changed from mostly conventional such as motors and filament bulbs to mostly non-linear loads that use switchmode power supplies (SMPS), electric drives and compact fluorescent lamps (CFL). That unfortunately for the power system has made the quality issue more serious. Power quality is anything that affects the voltage, current and frequency of power being supplied to the customers. Constant voltage is the prime requirement of the customer because if the voltage is lower than the tolerable limits it will cause overheating of the equipment and less illuminating power to the lighting load. If it is higher than the limit it causes material insulation break down, reduces the life of lighting load etc. Lightning (transient over voltages), switching over voltages (i.e. capacitor switching, disconnection of lines), short circuit faults (such as voltage sags) and short interruptions are the main causes for voltage deviations which lead to permanent damage of the equipment. Power system frequency is related to the balance between power generation and the load. When this balance changes, small change in frequency occurs. The frequency variations that go beyond acceptable limits for normal steady state operation of power system are normally caused by fault on the transmission lines, large portion of load being disconnected, or a large source of generation being isolated. Drop in frequency could result in high magnetizing currents in induction motors and transformers, causing problem of overheating and saturation. Off nominal frequency will cause damage to turbine and generator due to high vibration of turbine blades

which causes protection to trip out. Therefore it is essential requirement to maintain frequency of the system within the tolerable limits. Nowadays due to lot of harmonic injection in to the power system by the load that are also more sensitive in nature, the use of custom power devices/custom controllers (electronics based) to maintain power quality has become essential. As custom power controllers are used for current interruptions and voltage regulations, their utilization in the industry saves its equipment from voltage dips and interruptions which lead to loss of production. Minimize total harmonic distortion (THD) and improve the load power factor that minimizes the losses in the network. This chapter will present an overview of major power quality issues at the distribution level: voltage disturbances, harmonics, transients, unbalance and flickers. Moreover different solutions for mitigation of these issues by using custom power devices along with some case studies will also be presented.

### 1.1 Power quality Issues

Power quality issues occur due to different type of electrical disturbances that depends on amplitude and/or frequency. These disturbances are divided into short, medium or long term depending upon their duration. The power quality disturbances that most often occur at the distribution level are discussed below.

#### 1.1.1 Voltage Disturbances

Voltage disturbances are characterized by their duration and depth. Duration is the length of time for which the voltage remains below a threshold. The depth is characterized by the retained voltage, which is the voltage that persists during the voltage disturbance, as opposed to the voltage decrease. IEEE definition of voltage sag is described as a sudden and short duration reduction in RMS value of the voltage at the point of electrical system between 0.1 to 0.9 pu with duration

from 0.5 cycles to 1 minute. It is known as a voltage swell if there is an increase between 1.1 pu and 1.8 pu in RMS voltage at the power frequency for durations from 0.5 cycles to 1 minute. In case, the voltage is completely lost or is less than 0.1 pu in one or more phase conductors for a period between 0.5 cycles and 1 minute than it is known as interruption. Any disturbance that persists for less than 0.5 cycles is considered a transient phenomenon while the one that is longer than 1 minute could be overvoltage, undervoltage or sustained interruptions depending upon the RMS voltage magnitude greater than 1.1 pu, less than 0.9 pu or completely lost or less than 0.1 pu respectively. These voltage disturbances are categorized in the Figure [fig: VoltDisturb] with respect to RMS voltage and time duration of the disturbance. Short duration voltage disturbances mostly depend upon the location of the fault and also on the condition of the power system. Figure [VoltDip] and [VoltIntp] show some fault events [1]. [float Figure:[Figure 1. 1: Categorization of Voltage disturbances.]

Voltage sags occur a lot in a power system that's why they are considered the most severe disturbance to industrial equipment. Disturbance of only 10% sag for duration of 100ms can affect the quality of papers in paper mill [3]. In case of semiconductor industry, voltage sag of 75% (of the nominal voltage) with duration shorter than 100ms results in material loss in the range of thousands of U. S dollars [2]. The cause of voltage sag could be due to different events in the power system like short circuit faults in the transmission and distribution system, starting of large Induction motor or

transformer energizing can also result in shallow dips [4].

Figure 1.2: (a) Voltage Dip and (b) Voltage Interruption events.

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Figure 1.3: Faults on parallel feeder causing voltage sag

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In case of three phase voltage sag due to a fault at the point of common coupling (PCC) in a radial system, as shown in Figure 1.3. The Voltage divider model can be used for the calculation of voltage sag magnitude. In this case voltage  $\overline{E}_g$  during fault can be expressed as  $\overline{E}_g = \frac{\overline{Z}_f}{\overline{Z}_g} \overline{E}_s + \overline{Z}_f \overline{E}_s$  Where  $\overline{Z}_g$  is the impedance of the grid,  $\overline{Z}_f$  is the impedance between the PCC and the fault including fault and line impedances and  $\overline{E}_s$  is the supply voltage.

Voltage sag is also related to the changes in voltage phase angle. This change in phase angle is also called as phase angle jump (i. e. the phase angle between during sag and pre-sag voltages) and is obtained by taking

argument of the complex of voltage  $E_g$  [5]. Long duration voltage variations are mostly due to inadequate voltage regulation, equipment malfunction or failure or switching of large loads in a power system. Figure [Overvoltage] presents an overvoltage caused by a transformer failure. Figure [sustainedIntp] presents a sustained interruption due to the operation of a line circuit breaker. These disturbances are often permanent and require human intervention for system restoration [6].

Figure a:

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[float Figure:[Sub-Figure b:

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[Figure 1. 4:(a) Overvoltage due to transformer failure (b)

Sustained Interruption due to malfunction of equipment.

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1. 1. 2 Harmonics According to the IEEE definition harmonics are sinusoidal voltages or currents having frequencies that are integer multiples of the frequency at which the supply system is designed to operate (termed the fundamental frequency; usually 50 Hz or 60Hz). Both the voltage and current harmonics are measured in terms of total harmonic distortion (THD) at the PCC, which is the point where other customers can be connected with

the electric utility. And the quoted values are explicitly specified as voltage and current values. Conventionally, current distortion measurements are suffixed with ' I', e. g. 30 % THDI, and voltage distortions suffixed with ' V', e. g. 5 % THDV. Figure 7 shows a fundamental sine wave with 60% 3rd and 40% 5th harmonics. [float Figure:

## **[Figure 1. 5: Fundamental with 3rd and 5th harmonics.**

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When talking about harmonics in power installations it is the current harmonics that are of more concern because the harmonics originate as currents and most of these waveform distortions are due to these currents [8. 1]. Because of which stricter limits are imposed by electrical utilities [7]. When harmonics currents from the different sources produce a drop across the impedance network; they distort the voltage at that point. Another harmonic phenomenon is due to the shunt or series resonance in the network that can cause a voltage magnification [8]. But the most important reason that is also a concern for the future electrical utility is the way the loads draw current from the utility, which introduces harmonics in the system these are non-linear loads. Figure [nonlinear loads] shows the current drawn by different non-linear loads. These currents result in distorted voltages that further affect the other loads in the system. As the number of harmonic producing loads has increased over the years, it has become increasingly necessary to address their influence when making any additions or changes

to an installation [9]. [float Figure: Harmonic currents of different non-linear loads.

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Normally the power system distribution is able to absorb the harmonic produced by the loads that satisfy the IEEE Std 519-1992 limits at the PCC [10]. But it is the combined effect of many loads at the PCC that could cause the harmonic distortion of main supply voltage, which can lead to energy losses due to unwanted current in the system. As clearly visible in the Figure 7 and 8, the sum of the fundamental, 3rd and 5th harmonic that gives high peaks that are phase dependent, which may result in defective operation of regulating devices, malfunction of protective relays or circuit breaker and other control systems. High harmonic amplitude may also overload the power distribution network thus reducing its power transfer capability and overheat the neutral conductor because of skin and proximity effects, which increase with frequency and dielectric breakdown may occur causing it to burn out [11- 13].

### 1. 1. 3 Voltage Unbalance

In simple terms, voltage unbalance is a voltage variation in a power system in which the voltage magnitudes are not equal or the phase angle differences between them is not 120 degree. In reality this is impossible to achieve in a power system. Before going into any formal definition of unbalance system we first have to know how to quantify an unbalance voltage or current in a three-phase system. This is done by mathematically breaking down the unbalance system into three symmetrical components. That are the positive-sequence, negative-sequence and zero-sequence components indicated by subscripts 1, 2, 0.

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0 respectively, shown in the Figure [unbalance]. They are calculated using matrix transformations of the three-phase voltage or current

phasors. 
$$\begin{bmatrix} U_0 \\ U_1 \\ U_2 \end{bmatrix} = \frac{1}{3} \begin{bmatrix} 1 & 1 & 1 \\ 1 & a^2 & a \\ 1 & a & a^2 \end{bmatrix} \begin{bmatrix} U_a \\ U_b \\ U_c \end{bmatrix}$$
 Where

the rotation operator  $a$  is given by:  $a = e^{j120^\circ}$

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[float Figure: [Figure 1. 7: Positive, negative and zero sequence components

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For a perfectly balanced system both negative and zero sequence systems would be absent. These sequence systems can be given some physical interpretation. The direction of rotation of a three-phase induction motor when applied with a negative sequence set of voltages is opposite to what is obtained when the positive sequence voltages are applied. Having no phase displacement between the three voltages in the zero sequence system, when applied to a three-phase induction motor, it will not rotate at all as there will be no rotating magnetic field. According to the IEEE definition of voltage unbalance its defined as the ratio of the negative or zero sequence component to the positive sequence component. This is also known as negative sequence unbalance factor (NSUF). And it is considered to give the true unbalance in the system. 
$$\%, NSUF = \frac{U_2}{U_1} * 100$$
 Where  $U_1$  and  $U_2$  are positive and negative sequence components of three-phase line voltages can be calculated using equation above. According to The

National Electrical Manufacturers Association (NEMA) the voltage unbalance is as follows: 
$$\text{VoltageUnbalance} = \frac{\text{Maximum deviation from the mean of } \{U_{ab}, U_{bc}, U_{ca}\}}{\text{Mean of } \{U_{ab}, U_{bc}, U_{ca}\}}$$
 Line-neutral voltages should not be used with equations (1) and (2) as the zero sequence components can give incorrect results. Although both definitions give different results but the analysis in [17] shows that it is not significant up to 5% voltage unbalance. The main cause of voltage unbalance is the lack of symmetry in the loads at the LV distribution network. Due to large single-phase loads like arc furnaces and welders connected at the distribution network that makes the system unbalanced. Also due to the rapid increase in the small distributed generations like PV panels that are connected to low voltage distribution network through a single phase power electronics converter. These small generations have high impedance and low short circuit power that result in a large unbalanced voltages. Moreover faulty power factor correction capacitor banks, and open delta or wye transformers also contribute to unbalanced voltage. Abnormal system conditions that typically include phase-to-ground, phase-to-phase and open conductor faults also cause phase unbalance. The most common victim of unbalanced voltages is the electric motor that happens to be the work horse of the modern industry. Unbalanced voltage in an induction motor will reduce its efficiency and cause heating in the windings that will reduce the life of insulation and hence the motor life [21]. Even the NEMA premium efficiency motors are built for voltage unbalance of 1% [20]. Furthermore it also decreases the capacity of the cables and transformer in power system due to negative sequence. In case of transformer if the delta configuration is used

the zero sequence will circulate and cause heating [18]. AC variable speed drives and converters normally draw non-linear current that injects harmonics in to supply due to the unbalance voltage these harmonics increases because the current becomes more non-linear [19].

#### 1. 1. 4 Transients

In IEEE Std 100-1992 another synonymous used for transients is surge. It is defined as " a transient wave of current, potential, or power in an electric circuit." Based on the wave shape of the transient current or voltage the transients can be classified into two main categories, impulsive and oscillatory transients.

Impulsive Transient is one of the two types of transient disturbance that may enter the power system. It is defined by IEEE as a sudden, non-power frequency change in the steady-state condition of voltage, current, or both that is unidirectional in polarity - either primarily positive or negative. It is normally a single, very high impulse like lightning. Currents produced from a lightning strike can go to several thousand amps in about 2-3 $\mu$ s. Impulsive transients are generally described by their rise and decay times. They can also be characterized by their spectral content. Impulsive transients are not usually transmitted far from the source of where they enter the power system. However, in some cases, they may propagate for some distance along distribution utility lines. Also, it may considerably have different characteristics when viewed from different parts of the electrical system. In addition, the high frequencies involved allow damping of the impulsive transients through the resistive component of the system.

Electrostatic Discharge is another form of an impulsive transient. Most of us are familiar with this, since we may have already experienced such when touching an object like door knob or another person, after walking across a carpeted floor.

The sudden release of charge can damage sensitive electronics. This is the main reason why technicians use wrist straps when servicing electronic equipment. The effects of transients on a power system depend on the amplitude of the transient and its frequency. In the case of impulsive transients, its amplitude is the main cause of problems. The damage caused by a transient can be immediate (i. e. lightning strike). It can also be gradual as in the case of low-amplitude transients, which slowly degrade equipment insulation making it prone to short circuit [22].

Oscillatory Transient is described as a sudden, non-power frequency change in the steady-state condition of voltage, current, or both that has both positive and negative polarity values (bidirectional). In other words, the instantaneous voltage or current value of an oscillatory transient varies its polarity quickly. It is described by its spectral content or predominant frequency, magnitude and duration. The oscillatory transient is subdivided into three classes. These are based on selected frequency ranges, which correspond with common types of power system oscillatory transient phenomena. It should also be noted that the frequency of the oscillation gives a trace to the origin of the disturbance [25].

According to the classification given in IEEE Standard 1159-1995, an oscillatory transient with a primary frequency component less than 5 kHz, and duration from 0.3 ms to 50 ms, is considered a low frequency transient [27]. These transients are normally encountered on subtransmission and distribution systems that could originate primarily due to capacitor bank energization. Electric distribution utilities use capacitor banks to improve power factor, as well as lower system losses. For better results, capacitor banks have to be switched in and out of the system to match with

changes in the load profile. However, capacitor bank energization yields an oscillatory voltage transient with frequencies between 300 and 900 Hz [23-24], Figure shows this effect. Also, oscillatory transients with fundamental frequencies less than 300 Hz can be observed on the distribution system due to transformer energization and ferroresonance. In addition, series capacitors may also produce this transient type when the system resonance causes the magnification of low frequency components in the transformer inrush current or when unusual conditions lead to ferroresonance. An oscillatory transient with a predominant frequency component between 5 and 500 kHz and a duration measured in tens of microseconds is termed a medium frequency transient. Back-to-back capacitor switching is a typical example of these transients [26]. It occurs when a capacitor bank is switched in close electrical proximity to another capacitor bank that is already energized, which sees the de-energized bank as a low impedance path. Other causes of this type of transient include cable switching and as a system response to an impulsive transient. Oscillatory transients with a predominant frequency component greater than 500 kHz and a typical duration in microseconds are considered high frequency transients. This type of transients are linked with power electronics and switching events such as linear cable energization. Power electronics, like the SMPS in computers, generate oscillatory voltage transients that repeat several times the system frequency. Usually, they are also the result of a local system response to an impulsive transient.

1. 1. 5 Voltage Flickers [float Figure: [float Figure: [Sub-Figure a:

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[float Figure:[Sub-Figure b:

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[Figure 1. 8:(a)Voltage flicker due to an arc furnace and (b) transient due to capacitor switching.

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A random or repetitive variation in the RMS voltage between 0.9 pu and 1.1 pu, which cause rapid visible changes of light level in lighting equipment is known as flicker. The term flicker is derived from the impact of the voltage fluctuation on lighting intensity. Voltage flicker can be separated into two types: cyclic and noncyclic. Cyclic flicker is a result of periodic voltage fluctuations in the system voltage, with noncyclic referring to occasional voltage fluctuations. The main cause of voltage changes is the time variability of the reactive power component of fluctuating loads. In general, voltage flicker occurs on relatively weak systems with a low short-circuit capacity. So the loads with a high rate of change of line current in a short time can result in a flicker [28]. Arc furnaces are the most common cause of voltage fluctuations on the transmission and distribution system, see Figure [flicker]. Also note that small power loads such as starting of induction motors, welders, boilers, pumps and compressors, cranes, elevators etc. can also be the sources of flicker [28. 1]. Capacitor switching and on-load

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transformer tap changers that can change the inductive component of the source impedance are also a cause of flickers [34]. Variations in generation capacity like, in wind turbines can also have an effect. In some cases, voltage fluctuations can be caused by low frequency voltage inter-harmonics [33]. Voltage fluctuations have an effect on wide range of equipment and devices that are commonly used in industry. In an induction motor these fluctuations can cause changes in torque and slip and in a worst case scenario that may lead to excessive vibrations that will reduce the mechanical strength of the motor [31]. In phase-controlled rectifiers with dc-side parameter control usually it is a reduction of power factor and the generation of non-characteristic harmonics and inter-harmonics. In an inverter during drive braking commutation failure could occur due to flickers [32]. In order to protect equipment from unexpected failures and damages the voltage fluctuation measurements are required to determine actual load emission levels for comparison with limit values given in [29-30].

**Mitigation of Power Quality Issues** For the mitigation of the power quality issues whether it's the customer or the power utility the economic factor is very important. Most often no one is interested in investing until the power quality issue becomes serious. In order to save huge investment latter the best solution is to manage power quality from the very beginning at the equipment level rather than at the PCC. For mitigation of PQ issues custom power devices are used. These devices include both the passive and power electronics devices that are able to react in real time to the state of the distribution system and adjusting itself to maintain the required level of power quality. The decision to choose between different custom power

controllers is based on particular PQ issue, size of sensitive load, geographic location and the condition of the electrical network based on this data a cost analysis is done to find the most suitable solution. Nowadays due to more sensitive nature of loads use of custom power devices that are electronics based to maintain power quality has become essential. The key technology that has made custom power devices possible is the solid-state switch like the gate turn-off thyristor (GTO), the insulated gate bipolar transistor (IGBT), and the integrated gate commutated thyristor (IGCT). These devices have the operational capabilities suitable for high power applications at a cost that makes them economically possible for distribution power levels. In this section the passive and power electronic based custom power devices for voltage sags that are regarded as one of the most harmful power quality (PQ) disturbances due to their costly impact on industrial processes, harmonics that are rapidly increasing due to the use of non-linear loads and the voltage unbalance that affects the electric motor that is the work horse of the modern industry are discussed.

### 1. 2. 1 Passive Mitigation Devices

In the following section, the passive custom power for voltage dip, harmonics and unbalance mitigation as shown in Figure [passiveMit], are discussed briefly:

[float Figure: Passive mitigation devices for voltage sag, harmonics and unbalance.]

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### 1. 2. 1. 1 Voltage Dip Mitigation Ferro-resonant Transformer

The purpose of the Ferro-resonant transformer is to provide constant output voltage despite of changing in input voltage and load. Sometimes these transformers are also

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called as Ferroresonant or CVTS (constant voltage transformers) [37]. In actual design of this transformer as shown in Figure [FRTa] the capacitor is connected to the secondary winding of the transformer to set the operating point above the knee of the saturation curve, Figure [FRTb]. These kinds of transformers are only used for low-power; constant loads because variable loads can cause problems, due to the presence of tuned circuit on the output.

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[Figure 1. 10:(a) Single line diagram of Ferro-resonant transformer and (b) the saturation curve of transformer.

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Static Var Regulator (SVR) The first static tap-changer in the world was used in the field operation in Norway in 1986 by ABB components [38]. It is used to avoid voltage sag. In this kind of the transformer thyristor based tap changer can be mounted on its secondary winding for the sensitive loads to change its turn ratio according to variations in the input voltage [39]. The Figure [SVR] shows the diagram of transformer with electronic tap-changer.

[float Figure: [Figure 1. 11: Single line diagram of Transformer with electronic tap-changer.

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The secondary winding feeds the load and its voltage regulation is accomplished by connecting and disconnecting different sections of the same winding by fast static switches in the steps. This fast switching of winding sections also results in transients because of change in winding inductance which is the drawback of this technique. Also note that this technique involves static switches so it can also be put in power electronics based voltage sag mitigation devices. Rotating machines (Motor-Generator set) Motor-Generator set consists of motor supplied by grid, asynchronous generator supplying the load and the flywheel; all are connected at a common axis. Three-phase diagram of motor-Generator set with flywheel is shown in Figure [MGset].

When motor rotates the rotational energy will be stored in the flywheel which is used to maintain voltage regulation during disturbances. This scheme has high efficiency and low initial cost but it can only be used in industrial environment due to its size, noise and maintenance requirements.

[float Figure: [Figure 1. 12: Three phase diagram of Motor-Generator set with flywheel.

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1. 2. 1. 2 Harmonic mitigation Phase Shifting Transformer Phase shifting transformers are the effective way to cancel out the 5th and 7th harmonic.

This method is clear and fundamentally easy to understand. The principal is

to take harmonics generated from separate sources, shift one source of harmonics  $180^\circ$  with respect to the other and then combine them together; this will result in cancellation. When load currents are not matched, the harmonics can be partially cancelled. It may be a single transformer with two separate windings (ie: delta and wye) as shown in Figure [PshiftingTran].

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(a) Three phase diagram of Dyd transformer and (b) single line diagram of tuned filter.

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Tuned Harmonic filter These harmonic filters are used to reduce the harmonic distortion in the supply system. A tuned harmonic filter is a device with two basic elements an inductor and a capacitor. These reactive elements are connected in series to form a tuned LC circuit. The tuned harmonic filter is connected as a shunt device to the power system as shown in the Figure [Tuned filter] below. The tuned harmonic filter is a resonant circuit at the tuning frequency so its impedance is very low for the tuned harmonic.

Because of the low impedance at the tuned harmonic frequency the tuned

filter now becomes the source of the tuned frequency harmonic energy demanded by the loads, rather than the utility. The filter impedance at the tuning harmonic behavior is like a resistor; below the tuning frequency it has a capacitive behavior, while the impedance above the tuning frequency has an inductive behavior. Due to the capacitive behavior at below the tuning frequency, the filter improves the displacement power factor. At the tuning frequency the filter acts like a very low resistance, and a great amount of harmonic current at this frequency flows through the filter and the total harmonic current distortion in the upstream system decreases. And the harmonic currents flow between the filter and loads. This decrease in the total harmonic current distortion improves the distortion power factor and thus the total power factor [35].

**Low Pass Filter** Low pass harmonic filters are popular due to their ability to attenuate all harmonic frequencies and achieving low levels of residual harmonic distortion. There are several circuit configurations available for the low pass filters. Typically, low pass filter configuration includes one or more series elements plus a set of tuned shunt elements as shown in Figure [LPF].

[float Figure:[Figure 1. 14: Single line diagram of Low pass filter.

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There are three parts input side, the shunt part and output the load side. The purpose of input stage is to isolate the LPF from other harmonics sources connected to the same power source and to prevent power system resonance. This stage also protects the load and filter capacitors against transients. The output stage contains a precise amount of impedance that

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minimizes the amount of harmonics produced by the load. It also reduces the harmonic burden placed on the shunt stage, and prevents resonance between the shunt stage and the load. The shunt stage absorbs residual harmonics remaining after both the input and output stages have played their roles in reducing load harmonics (primarily 5th and 7th). Our basic three stage filter design achieves the lowest possible harmonic distortion levels while preventing power system resonance. The low pass filter forms a hybrid combination of series and shunt elements that can be applied without performing system harmonic analysis. IGBT Based fast switching harmonics filter This harmonic mitigation technique is useful in situations involving dynamic loads with rapidly changing demands for reactive power. These filters are switched very rapidly IN and OUT of the circuit using IGBT's instead of contactors. This type of filter is also capable of soft switching the capacitor suppressing voltage spike. It can be switched, without discharging the capacitors, at switching rates up to 60 times per second. The main advantages of this filter are the capability to switch without transients and to respond in real time, to dynamically changing load conditions. The performance of the fast switched filter is similar to the performance that can be expected from a typical tuned filter, a total harmonic current distortion from 3 to 12% [35].

1. 2. 1. 3 Unbalance Mitigation

Scott-transformer This transformer transforms three phase power to two-phase power. It consists of two single phase transformer with a special winding ratio. One of the two single phase transformers has a middle-tapped winding on its primary side, and a single winding on its secondary side. Figure shows the scott connection scheme. They are connected in such

a way that at the output, a two-phase orthogonal voltage system is generated allowing the connection of two single-phase systems. This setup draws a balanced three-phase power from the grid.

[Sub-Figure a:

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[float Figure:[Sub-Figure b:

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[Figure 1. 15:(a) Schematic diagram of scott-transformer and (b) the singleline diagram of steinmetz transformer for induction furnace.

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Steinmetz-transformer It is a three-phase transformer with an extra power balancing load, consisting of a capacitor and an inductor that are rated proportional to the single phase load, Figure shows the steinmetz transformer for load balancing in a large induction furnace load. When the reactive power rating of both the inductor and the capacitor is equal to the active power rating of the load (divided by root 3) then the three-phase grid sees a balanced load. The three-phase rated power of the transformer is equal to the single-phase active power of the load. This balancing is only perfect for loads with an active power equal to the value used to design the system. The detail calculation using steinmetz transformer

can be found in [36].

1. 2. 2 Power Electronics based mitigation devices

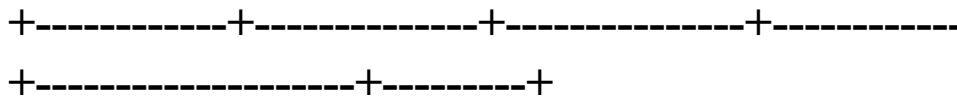
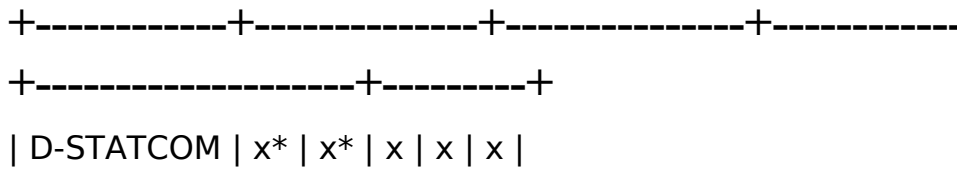
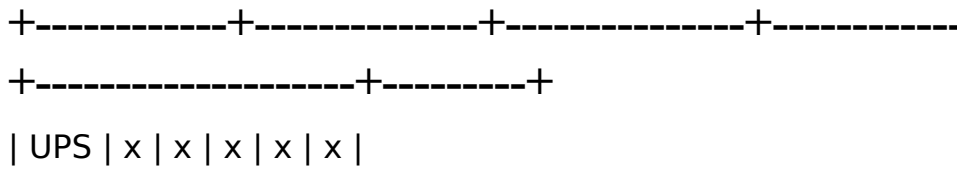
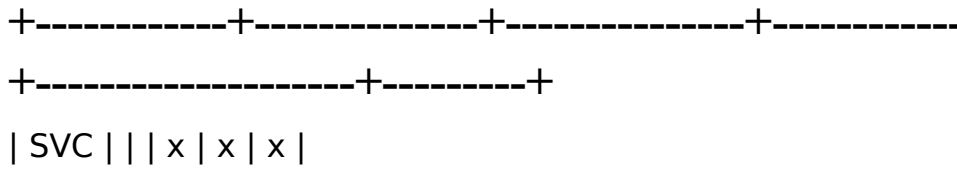
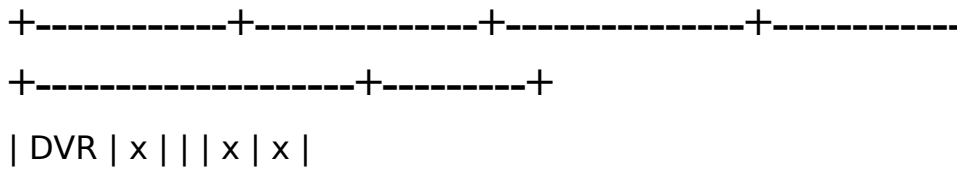
At the heart of the custom power devices that are power electronics is a three-phase voltage source inverter. The inverter is controlled by a digital system that constantly monitors the distribution line and controllers the output according to some control algorithm. The inverter is connected to the distribution line via a filter that removes the harmonics injected by the inverter and a transformer for isolation. The inverter itself could be a 2 level PWM or multi-level inverter. The custom power devices that can inject active power need an energy storage that could be capacitors, batteries, flywheel or superconducting magnetic energy storage (SMES). Table [Active Devices] shows some of the power electronic based custom power devices for mitigating voltage dips, interruptions, harmonics, unbalance and flicker. These devices are briefly discussed in the following section.

Table: [Table 1. 1: Summary of mitigation capability of various power electronics based custom power devices.

Devices	Voltage Dip	Interruption	Harmonics	Voltage Unbalance	Flicker

| STS | x | x | | | |

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[footnote:\* Only if energy storage is present.

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1. 2. 2. 1 Static Transfer Switch (STS)The static transfer switch (STS) is an electrical device whichallows the instantaneous transfer of the load from preferredsource to an alternative healthy source in case of the voltage disturbance. This means that if one power source fails STSwitches to the back-up power source quickly in such a way thatload never realizes any disturbance. Figure [STS]shows singleline diagram of Static Transfer Switch (STS).[float Figure:[Figure 1. 16: Single line diagram of STS.



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Normally, static switch on the primary source is fired regularly, while the other one is off. It is generally used to mitigate voltage sags and interruptions in the distribution system but it cannot protect against the sag originating in the transmission system.

### 2.2.2 Uninterruptible Power Supply (UPS)

The main purpose of uninterruptible power is to provide uninterruptible, reliable, and high quality power to the loads. UPS consists of rectifier which is supplied by grid, battery and the inverter which supplies the load. Figure [UPS] shows three-phase diagram of UPS. The rectifier is used to convert ac voltage into dc which supplies power to the inverter as well as battery bank to keep it charged. In normal operating conditions, battery gets charged and power is supplied to the inverter by rectifier. In case of an outage, battery bank supplies the power to the load [40]. Depending upon the storage capacity of the battery, it can supply the load for minutes or even hours. UPS is a low power application device and is used in medical equipment, data storage and computer system, emergency equipment, telecommunications and online management systems [41]. For higher-power loads the costs associated with losses due to the two conversions and maintenance of the batteries become too high and, therefore, a three-phase, high power UPS is not economically feasible.

[float Figure: [Figure 1. 17: Three phase diagram of UPS.

]

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1. 2. 2. 3 Shunt connected Voltage source Converter (D-STATCOM)The Distribution Static Compensator (D-STATCOM) is a shuntconnected voltage source converter based static compensator which is used for voltage regulation at the PCC and reactive power control by injecting controlled amount of current  $\underline{i}_r(t)$  of desired amplitude, frequency and phase into the grid. The typical configuration of a STATCOM is shown in Figure [Dstatcom1]. This device consists of a VSC, an injection transformer, an AC filter and a DC-link capacitor. The line impedance has a resistance  $R_g$  and inductance  $L_g$ . The grid voltage and current are denoted by  $\underline{e}_s(t)$  and  $\underline{i}_g(t)$ , respectively. The voltage at the PCC, which is also equal to the load voltage, is denoted by  $\underline{e}_g(t)$  and the load current by  $\underline{i}_l(t)$ . The inductance and resistance of the AC filter reactor are denoted by  $R_r$  and  $L_r$ , respectively.

Figure: [Figure 1. 18: Single line diagram of shunt connected VSC.

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By injecting a controllable current, a STATCOM can limit voltage fluctuation leading to flicker [42] and cancel harmonic currents absorbed by the load, thus operating as an active filter [43]. In both cases, the principle is to inject a current with same amplitude and opposite phase as the undesired components in the load current, so that they are cancelled in the grid current. These mitigation actions can be accomplished by only injecting reactive

power. [float Figure: [Figure 1. 19: Phasor diagram of D-STATCOM  
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A STATCOM can also be used for voltage dip mitigation if energystorage can also be mounted on the DC link to allow active powerinjection into the AC grid. In this case, the device has toinject a current in the grid which results in an increasedvoltage amplitude at the PCC, as shown in the phasor diagram inFigure [Dstatcom2]. The voltage phasor at PCC is denoted by

$\overline{E}_g$ ,  $\overline{Z}_g$  is the line impedance,  $\overline{E}_{s, dip}$  is the grid voltage phasor during the dip and  $\psi$  is the phase-angle jump of the dip. From the diagram it is possible to understand that when the shunt-connected VSC is used to mitigate voltage dips, it is necessary to provide energy storage for injection of active power in order to avoid phase-angle jumps of the load voltage. If only reactive power is injected, it is possible to maintain the load voltage amplitude  $E_g$  to the pre-fault conditions but not its phase [41. 1]. Therefore, the voltage dip mitigation capability of a shunt-connected VSC depends on the rating of the energy storage and on the rating in current of the VSC. One drawback of using D-STATCOM for voltage dip mitigation is a high rating of voltage source converter. To restore the load voltage to the pre-fault conditions (without introducing phase-jump), the following condition must be fulfilled  $\overline{E}_g = \overline{E}_{s, dip} + \overline{Z}_g \overline{I}_r$  Active and the reactive power injected by the device can be calculated in per unit as  $P_{inj} = \frac{\cos\varphi_g}{Z_g} \left( \overline{E}_{s, dip} \cos(\varphi_g - \varphi_s) - \overline{E}_g \cos(\varphi_g - \varphi_s + \psi) \right)$   $Q_{inj} = -\frac{\sin\varphi_g}{Z_g} \left( \overline{E}_{s, dip} \sin(\varphi_g - \varphi_s) - \overline{E}_g \sin(\varphi_g - \varphi_s + \psi) \right)$

$\{E_{s, dip} Z_g\}$  where the source voltage, the line impedance and the load impedance are expressed as  $\overline{E}_s = E_s e^{j\varphi_s}$ ,  $\overline{Z}_l = Z_l e^{j\varphi_l}$  and  $\overline{Z}_g = Z_g e^{j\varphi_g}$ , respectively.

1. 2. 2. 4 Dynamic Voltage Restorer (DVR)

Dynamic Voltage restorer (DVR) is series connected voltage source converter based compensator which is used to inject voltage  $\underline{e}_c(t)$  of controllable amplitude and phase angle between the PCC and the load in series with the grid voltage through injection transformer to compensate for voltage dips. It is connected in series with a distribution feeder and is used to generate or absorb active and reactive power at its ac terminals. The first DVR was installed for rug manufacturing industry in North Carolina [44]. Another was used in Australia for large dairy food processing plant [44]. Figures [DVR1] and [DVR2] show the single line and simplified diagram of the Dynamic voltage restorer respectively. It is used to maintain load voltage  $\underline{e}_l(t)$  to the pre-fault condition by injecting missing voltage of appropriate amplitude and phase.

[float Figure: [Figure 1. 20: Single line Diagram of DVR.

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[float Figure: [Figure 1. 21: Simplefied diagram of DVR.

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[float Figure: [Figure 1. 22: Phasor diagram of DVR during voltage sag mitigation.

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Figure [DVR3] shows the phasor diagram of series injection principle during voltage dip mitigation,  $\overline{E}_l$  is the phasor of pre-fault load voltage,  $\overline{E}_c$  is the phasor of injected voltage by the device,  $\overline{I}_l$  is the phasor of load current,  $\varphi$  is the phase displacement from the load current and load voltage,  $E_{g, dip}$  is the dip in the amplitude of the grid voltage and  $\psi$  is phase angle jump. The DVR injects reactive power for compensation of voltage amplitude but it injects active power for correcting phase angle jump as well. Injection of active power by DVR is related to energy storage. DVR injecting larger amount of active power requires bigger size of energy storage leading to more

expensive scheme rather than injecting less amount of active power. This size of energy storage can be reduced by optimization of energy storage by using the techniques in [45]. Assuming the load voltage and current in pre-fault conditions is equal to 1 pu, the injected power by the device during voltage dip mitigation is equal to  $\overline{S}_{inj} = \overline{E}_c \overline{I}_l^* = (\overline{E}_l - E_{g, dip}) \overline{I}_l^* = (1 - E_{g, dip}) e^{j\psi} e^{j\varphi}$ . The Euler identity can be written as  $e^{j\varphi} = \cos\varphi + j\sin\varphi$ , applying to equation 2.2 we get  $\overline{S}_{inj} = \cos\varphi + j\sin\varphi - E_{g, dip} \cos(\varphi + \psi) - jE_{g, dip} \sin(\varphi + \psi)$ .  $\overline{S}_{inj} = (\cos\varphi - E_{g, dip} \cos(\varphi + \psi)) + j(\sin\varphi - E_{g, dip} \sin(\varphi + \psi))$ . Power absorbed by the load will be given by  $\overline{S}_{load} = P_{load} + jQ_{load} = \overline{E}_l \overline{I}_l^* = e^{j\varphi} =$

$\cos\varphi + j\sin\varphi$  Therefore the active and reactive power injected by the DVR are given by

$$P_{inj} = (1 - \frac{E_{g, dip}}{E}) \cos(\varphi + \psi)$$

$$Q_{inj} = (1 - \frac{E_{g, dip}}{E}) \sin(\varphi + \psi)$$

The main components of DVR are: Voltage source

converter (VSC) Generally pulse-width modulated voltage source converter is

used because of simplicity and good response. It is used to generate desired

voltage to be injected for the compensation. The basic function of VSC is to

convert DC voltage supplied by the energy storage into AC voltage and

vice versa so it can be said that it is a converter through which power flow is

reversible. When power flow is from DC to AC it is said to be in inverter mode

and when power flow is from AC to DC it is in rectifier mode. The valves in

converter are usually IGBTs, but some DVR manufacturers also use IGCTs

[46-47]. Series Injection Transformer The main purpose of

injection transformer is to increase the voltage supplied by LC filter and to

inject the missing voltage of the system at the load bus. For three-phase

DVR, three single-phase transformers are used for this purpose [48]. The high

voltage side of the transformer is connected in series to the line, while DVR

power circuit is connected to the low voltage side. The primary winding can

be connected in either star or in delta with the converter side. When three

single-phase converters are used, a connection of three windings of

transformer will be in wye to realize a four-wire configuration in order to

inject a zero-sequence voltage into the line. A delta connection increases the

injected voltage (in pu) with respect to the converter output voltage by

a factor of  $\sqrt{3}$  and have an advantage of blocking zero sequence currents that

may circulate in the feeder. To operate the injection transformer properly into

the DVR, MVA rating, turnsratio, the primary winding voltage and current ratings and shortcircuit values of transformer are required [48]. Energy storage An energy storage device is normally connected to the DC bus of the converter to provide the required energy for the compensation. Commercially available DVRs use large capacitor banks for the storage of energy [49]. This is the most expensive part of DVR. In normal operating condition it is charged through grid voltage and in case of disturbance it supplies energy to compensate for load voltage. Passive filter The nonlinear characteristics of semiconductor devices cause distorted wave forms associated with high frequency harmonics at the output of the inverter. To reduce these harmonics filter unit is used. Although PWM technique is used in the converter with high switching frequency which generates a voltage wave form with very low content of the harmonics, a second-order LC filter is used for further reduction of the harmonics in the injected voltage.

### 1. 2. 2. 5 Static var compensators (SVCs)

The purpose of a compensator is to measure adequate electric quantities of the load and generate in the compensator such currents, that the resultant load: compensator - compensated load, as seen from the supply network, was symmetrical, and the fundamental harmonic reactive current drawn from the network did not exceed the value permitted in the supply conditions. Generally, static compensators are the systems, which comprise reactors and/or capacitors controlled by means of semiconductor circuits.

### Thyristor Controlled Reactor (TCR)

The TCR operates as a gradually variable reactor, shown in Figure. It's just a reactor connected in shunt through a thyristor that can be controlled by continuously changing the firing angle  $\alpha$ , which changes the susceptance of the TCR, Figure

shows the V-I characteristics of TCR. In the V-I plane, it means "jumping" from one characteristic to the other - the whole range between  $\alpha = 0$  and  $\alpha = 90^\circ$  can be covered [6].

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[float Figure:[Sub-Figure b:

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[Figure 1. 23:(a) Single line diagram of TCR and (b) the characteristic curve of TCR.

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Fixed capacitor/thyristor controlled reactor (FC/TCR) The simplest way to realize continuous voltage regulation both in inductive and capacitive range is putting a capacitor in parallel with a TCR known as FC-TCR as shown in Figure . When TCR is off, we have only FC and when TCR is fully on, half of its current is taken by fixed capacitor. The range of regulation is always 1 pu, but now we regulate both  $E > V_{ref}$  and  $E < V_{ref}$  ]

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[float Figure:[Sub-Figure b:



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[Figure 1. 24:(a) Single line diagram of FC/TCR and (b) the characteristic curve of FC/TCR.

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]

FC/TCRs are employed where control requirements demand finer resolution that is not possible or economical with switched capacitor steps. For example, in applications where the shortcircuit ratio is low, very small compensation steps are needed to reduce flicker. A large number of small binary-switched capacitor steps would be required, increasing the cost and complexity of a solution that only used a fixed capacitor array. The FC/TCR combination can provide a more effective and lower cost solution when finer resolution is necessary. Thyristor switched capacitor (TSC) The TSC is used to inject reactive power into the grid. Similar to the TCR, it is constituted by an AC switch connected in series with a fixed capacitor. A small inductor is needed to limit the  $di/dt$  during switching operation. Using one TSC gives discrete variation of reactance with two operating points for each voltage value (TSC ON or OFF). Splitting the same total capacitance into more TSCs gives more operating points and higher controllability but increases cost. Also it is not possible to change the susceptance continuously to realize constant voltage. When the TSC is started, a resistor in series with the capacitors can ensure that they are charged slowly, thereby avoiding high inrush currents and system disturbances. After the capacitors are initially

charged, a contactor can automatically bypass the resistor.

Figure: [Sub-Figure a:

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[float Figure: [Sub-Figure b:

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[Figure 1. 25:(a) Single line diagram of TSC and (b) the characteristic curve of TSC.

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Thyristor controlled reactor/thyristor switched capacitor (TCR/TSC)

Figure: [Figure 1. 26: Characteristic curve of TCR/TSC.

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]

With a combined TCR/TSC compensator, continuously variable reactive power is obtained throughout the complete control range as well as full control of both the inductive and the capacitive parts of the compensator. This is a very advantageous feature permitting optimum performance during large disturbances in the power system. Also with the capacitor able to switch on/off by thyristors (TSC) the same resulting characteristic can be obtained with half the size of the reactor. It's a good solution when the voltage variations around  $V_{ref}$  are not big and when the same regulation range is

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needed in both inductive and capacitive regions. But the cost of the switches and the complexity of the algorithm for transient-free switching of the capacitor are few drawbacks for this solution.

### 1.3 Case Studies

This section presents some case studies where custom power controllers were installed to mitigate a power quality problem. Each case study presents a problem and the solution chosen along with the results after the mitigation.

#### 1.3.1 Case Study 1: Voltage Flicker mitigation using D-Statcom at Seattle Iron & Metals Corporation steel recycling facility in Seattle.

**Problem** In the year 1999 the Seattle Iron & Metals Corporation was a new steel recycling facility in Seattle, Washington. They have a huge 4000 hp shredder motor load that will be operating at this new facility. The distribution company Seattle city light has two substations to supply the plant, the South Substation and Duwamish Substation at 26.4 kV distribution network. But both feeders during the operation of the shredder motor gives voltage flicker at the PCC. The Figure shows the plant single line diagram with source impedance  $Z_1$ , feeder impedance  $Z_2$  and the transformer impedance  $Z_t$ .

[float Figure: [Figure 1. 27: System Configuration

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**Solution** The company provided the load fluctuation profile, shown in figure along with the flicker limitation as specified by IEEE std 1250-1995. The shredder motor specifications along with the max torque limit of the motor are also given in [1]. Only the voltage fluctuations caused by the shredder motor are considered in this study. The PCC for evaluating the voltage fluctuation is on the 4.16 kV bus on the low voltage side of the system

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supply transformer (5 MVA, 26.4 kV / 4.16 kV transformer), i. e., point C in Figure 5. Most effective way is to mitigate the problem at the source so that it doesn't affect the other loads in the distribution network. The measurement of voltage fluctuation is made to detect the 4.16 kV bus through a PT, and the rms value of line-to-line voltage of one phase is measured with a voltage transducer, which can be seen in Figure 8.

Table 1. 2: Load Fluctuation Profile and Flicker Limit

No	Load Condition	Load Current	Fluctuation Frequency	Upper Limit of $\Delta V$
1	200% load	2*FLA	1 hit/hour	2.7%
2	175% load	1.75*FLA	10 hit/hour	1.1%
3	150% load	1.5*FLA	20 hit/hour	0.9%

+-----+-----+-----+-----

+-----+

| 4 | 100% load | 1\*FLA | 20 hit/hour | 0. 9% |

+-----+-----+-----+-----

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| 5 | 50% load | 0. 5\*FLA | 1 hit/minute | 0. 7% |

+-----+-----+-----+-----

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| 6 | 25% load | 0. 25\*FLA | 5 hit/minute | 0. 5% |

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[footnote: FLA: Current at Load= 1 pu (= 450A)

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[float Figure:[Figure 1. 28: Mesurment System used

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[float Figure:[Figure 1. 29: Voltage fluctuation level at point C without compensation.

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After the measurement the voltage fluctuation with the feedersfrom both the substations, the supply from the south feederresulted in more voltage  
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fluctuation then Duwamish feeder, the results of the former are shown in figure[ ]. After considering the load fluctuation profile, the flicker limits shown in figure[ ] and the worst case voltage fluctuation that occurred when the south feeder was used, especially with the 200% FLA. The size of the D-Statcom is determined that is to be 5 MVA at 4.16 kV that will reduce the flicker level within the specified limit of 2.7% on the secondary of transformer, Figure [ ] shows the plant with D-Statcom. The results obtained after the D-Statcom installed to compensate the voltage flicker at the low voltage side of transformer are very convincingly within the specified limits, Figure[ ] shows these results. [float Figure: [Figure 1. 30: Voltage fluctuation level at point C with compensation.

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[float Figure: [Figure 1. 31: System with D-Statcom installation at point C.

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1. 3. 2 Case Study 2: Voltage Sag mitigation using a 4MVA DVR at Caledonian paper's manufacturing plant in Ayrshire. Problem Caledonian paper's manufacturing plant in Ayrshire is part of the UPM-Kymmene Group that is one of the largest manufacturers of lightweight coated (LWC) paper in the world. The supply to the plant is taken from the Scottish Power (a power utility company) 132 kV transmission system that has an inherent power quality issue of voltage disturbances. The paper machine process requires precise control of the paper sheet tension as it progresses through

the machine. On Caledonian Paper's paper machine this is achieved by controlling 23 separate DC variable speed drives, which are inherently vulnerable to voltage disturbances because of problems with the control of thyristor firing. Firing angle control has difficulty following the voltage change, with possible consequential damage to the thyristors. To prevent this damage, it is common for drives to be equipped with protection that trips the drive, using settings dependent on the drive's sensitivity to voltage disturbances. The manufacturer designed the software voltage trip threshold in the drives at 90%, so that disturbances below this level for more than a few cycles cause a trip. According to the monitoring carried out on Scottish Power's transmission and distribution system, and also within the paper mill, it was confirmed that the paper machine could be affected by disturbances of only 10% variation from normal (90% voltage retained) and for as little as 100ms. So in case of a voltage disturbance that results in the tripping of DC drive, the paper machine suddenly stops in an uncontrolled manner with the potential for extensive damage particularly, in the wire and press sections. In these sections the wires, rolls, associated felts and paper sheet all go out of control at high speed due to the voltage disturbance and, apart from the immediate interruption to production, the situation demands time-consuming clean up and inspection of equipment and machinery. If there is damage, depending on the part and extent of the damage, it can take several hours to restore production to original levels. Wasting valuable time and costing in both material and labor.

[float Figure: [Figure 1. 32: Single line diagram of Caledonian paper's manufacturing Plant.

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Solution On Scottish Power's transmission system, the best clearance times for protection and circuit breakers is 80-150ms, are not fast enough to prevent possible disturbances to paper machine production. However, the severity of any disturbance event is subject to the 'geography' of the power system between the plant and the fault location. Since the plant has a connection from the 132kV transmission system it is not exposed to the fault occurring in the distribution level. Different possible solutions like changing the tripping threshold of the drives that improved the drive resilience but did not provide a complete solution. Use of the UPS also not considered due to high load and short ride through requirement. Based on the size, cost and the suitability DVR became the preferred option. Next the DVR size need to be selected based on voltage disturbance statistics of the site, its duration and depth, the total size of sensitive load in the plant and its sensitivity limit. After considering the above factors the mill distribution system need to be segregated into critical and non-critical groups with critical load of 8.2 MVA, shown in Figure . Thus the 4 MVA (2\*2MVA units in parallel) DVR were installed to provide 50% injection for a duration of 300msec using 800kj of capacitance as energy storage. Figure shows an event recorded in an overhead line fault due to lightning and the DVR has retained voltage at the planned level of 95% voltage enabling the plant ride through of voltage sags. Table shows different recorded compensations by DVR. [float Figure: [Figure 1. 33: Single line diagram of manufacturing plant after the DVR installation.



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[float Figure:[Figure 1. 34: An event mitigated by the installed DVR.

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[float Table:[Table 1. 3: Disturbances compensated by the DVR.

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| Date | DVR input voltage retained (%) | DVR input dip duration (msec) |

cause |

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| 03 Apr 98 | 89 | 320 | 11kV: neighbouring customer fault. |

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| 20 May 98 | 81 | 1600 | 33kV: lightning-double circuit overhead line fault. |

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| 01 Sep 98 | 83 | 115 | 275kV: lightning: ovehead line transient. |

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| 29 Nov 98 | 81 | 135 | 275kV: unkown ovehead line transient. |

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| 04 Jan 99 | 88 | 123 | 132kV: gales: overhead line transient. |

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| 04 Jan 99 | 89 | 84 | 132kV: gales: overhead line transient. |

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1. 4 Summary The key power quality issues that have significant impact at the distribution level such as voltage sag, interruption, voltage unbalance, harmonics, flickers and transients are discussed. The custom power devices that are used mitigate these issues both passive and power electronics based are briefly explained to highlight the advantages and disadvantages. Then two case studies of actual projects are presented explaining the problem and finally presenting the solution along with improved results after mitigation of particular power quality issue.