

3-phase systems and two-port networks critical thinking example

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3-Phase Systems

For a star connection, $V_{line} = 3V_{phase}$

$V_{line} = 400 + 10\phi V$ where $\phi = 2$. Therefore, phase voltage = $420/3 = 242.48 V$

$I_{phase} = V_{phase}/Z_{phase} = 242.48/20 \angle 37^\circ = 12.124 \angle -37^\circ A$

For a star connection, $I_{line} = I_{phase} = 12.124 \angle -37^\circ A$

Since the loads are identical in terms of impedance and phase, the net current at the neutral point would be zero. Therefore, the current in the neutral wire is also zero.

Power dissipated = $I_{phase}^2 R_{phase} = 12.124 \times 12.124 \times 20 = 2.939 kW$

Apparent power $S = 3 V_{line} I_{line} = 8.81 kW$

Reactive power $Q = 3 V_{line} I_{line} \sin\theta = 5.31 kW$

Power factor of the load = $\cos\phi = \cos 37^\circ = 0.79$

Right now, $\phi = \tan^{-1}x = 37^\circ$ which implies $x = 0.75$. Impedance offered by capacitor = $1/2\pi 50 C = 0.75$. This gives $C = 4.2 mF$

When the fuse in V_c supply line blows, the line current through that line now flows through the neutral = $12.124 \angle -37^\circ A$

Two-Port Networks: Task 1

1.

Figure 1: Given network

Figure 1 shows the given network which is of the “ π ” model, as represented in Figure 2. Let’s transform analyze this network in terms of Y parameters, to verify the design criteria.

Figure 2: “ π ” Model Representation

2. Corresponding equations for the model are:

This means that:

Finally,

3. Using the above equations, we can calculate the input current and output voltage as follows:

Output Voltage - I_1 represents the input current. From the given network specifications, $Z_1 = 1592.35\Omega$, $Z_2 = 10\text{ k}\Omega$ and $Z_3 = 1\text{ k}\Omega$. Therefore, correspondingly, $Y_1 = 0.628\text{ mS}$, $Y_2 = 10\text{ mS}$, and $Y_3 = 1\text{ mS}$. Now, substituting these values in the model, $Y_{11} = 1.628\text{ mS}$, $Y_{12} = Y_{21} = -1\text{ mS}$, and $Y_{22} = 11\text{ mS}$.

Now using this in the other equations for the model, with $V_1 = 4.5\text{ V}$, we get $I_2 = V_2/(\text{input impedance of load}) = V_2/50 = (Y_{21} \times V_1) + (Y_{22} \times V_2)$. This gives, $V_2 = 0.5\text{ V}$.

4. Direct circuit analysis, without using admittance parameters, yields more or less the same results.

5. The specification of output voltage being at least 2.5 V is not met.

6. For maximum power transfer, the load impedance should be equal to the output impedance of the network by maximum power transfer theorem. Thus $\text{load} = 50\ \Omega$.

Figure 3 gives the attenuator circuit, while Figure 4 gives the “t” model for z parameters for the network.

Figure 3: Attenuator system

Figure 4: “t” model z parameters

Below are the corresponding impedance parameter equations to design the network.

Using the above equations and given specifications,

$$V_1 = 2 \text{ V}; \text{ maximum } V_2 = 100 \text{ mV}$$

$$I_1 = 0.02 \text{ A}; \text{ maximum } I_2 = 2 \text{ mA}$$

This gives $0.02 Z_{11} + 0.002 Z_{12} = 2$ and $0.02 Z_{21} + 0.002 Z_{22} = 100 \text{ m}$.

But $Z_{12} = Z_{21}$ and assume this is equal to 10Ω . This gives $Z_{11} = 99 \Omega$ and $Z_{22} = -50 \Omega$.

Corresponding components can be used in the design, which have been tested using TINA simulation software.