

Composition of saturated and unsaturated soil biology essay

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Dirts have two chief signifiers saturated or unsaturated this depend on the grade of impregnation (the H₂O content) . If the grade of impregnation is about 100 % the dirt is saturated and if it is much lesser than 100 % the dirt is unsaturated. Therefore, saturated dirt has merely two stages solid (dirt) and H₂O, whereas the unsaturated dirt has three stages solid, H₂O and air and there is another stage has been added which is called contractile tegument which is the interface between air and H₂O (Fredlund and Morgenstern, 1977 ; Fredlund, 2006) . This difference in composing of saturated and unsaturated dirt leads to a difference in the mechanical behavior of these dirts. Because of the fact that unsaturated dirts represent the bulk of surface dirts on the Earth and therefore most of the foundations of the buildings are placed on this dirt.

For this ground applied scientists have to understand the mechanical behavior of unsaturated dirts. Knowing the behavior of unsaturated dirt enables applied scientists to foretell the hazard or the failure when edifices or roads are constructed on such these dirts. the effectual trial that can be used to acquire cardinal apprehension of the mechanical behavior of unsaturated dirt is triaxial trial (Bishop and Donald (1961) ; Matyas and Radhakrishna (1968) ; Alonso et Al. (1987) ; Fredlund and Rahardjo (1993) ; Sharma (1998) ; Gallipoli et Al.

(2003) ; Wheeler et Al. (2003) ; Lu and Likos (2004) ; Sharma et Al. (2004)) .

Background

The cloth in unsaturated dirt is more of import than in concentrated dirt, because in concentrated dirt the cloth will be damaged instantly if the dirt is subjected to compaction or shear force. Whereas, the suction will back up the cloth in unsaturated dirt if it is subjected to shear or compression force this had been provided by (Toll, 1990). The pore H₂O in an unsaturated dirt will take three signifiers (bulk H₂O, adsorbed H₂O and semilunar cartilage H₂O). The adsorbed H₂O is the H₂O surfacing the dirt atoms. The H₂O is flooded in the null infinite is called bulk H₂O and the H₂O which surrounds the atom contacts is called meniscus H₂O.

Wheeler and Karube (1996)The H₂O semilunar cartilage which is shaped between neighboring atoms of unsaturated dirt is subjected to negative pore H₂O force per unit area (tensile emphasis) this will bring forth a normal force between the neighbouring atoms, This phenomenon, is called dirt suction, which can better the stableness of Earth constructions (Kayadelen et al. , 2007). An inter-particle contact force within bulk H₂O is likely to be different within the semilunar cartilage H₂O Wheeler et Al. (2003). The saturated dirt become unsaturated when the rate of vaporization is more than the rate of rain autumn and therefore H₂O tabular array will fall down and the dirt above the H₂O table becomes unsaturated. In add-on, unsaturated dirt can be formed by compaction.

? ? The dirt near to the land surface which is in a dry ambience or capable to compression processes this leads to unsaturated conditions and as a therefore subjected to negative pore H₂O force per unit area (Fredlung and

Rahardjo, 1993) . The mechanical behavior of the dirt can be divided for two parts by the land H₂O tabular array as it is shown in the figure (1) . The first portion is the dirt below the H₂O tabular array (the saturated dirt) which it ' s behavior is depend on effectual emphasis and the 2nd portion is the dirt above the T land H₂O tabular array (unsaturated dirt) which it ' s behaviour depend on independent matric suction and emphasis normal emphasis (Jennings and Burland, 1962, and Fredlund and Morgenstern, 1977) .

Capillary

The definition of capillary phenomena is the motion of H₂O in the connected nothingness infinites as a consequence of coherence, the forces of adhesion, and surface tenseness. The capillary is difference in force per unit area between the air and H₂O moving on the interface between air and H₂O (the contractile tegument)The capillary force which is produced by the surface tenseness go oning between H₂O and air leads to maintaining H₂O near to the contact point of two atoms. The capillary phenomena is seen when a little tubing is put in H₂O. The H₂O rises in the tubing due to the surface tenseness. As it is shown in the undermentioned figureThe tallness of H₂O in the tubing depend on the radius of the tubing, the value of the surface tenseness and the contact angleAt perpendicular force equilibrium: Where: is the tallness of H₂O in the tubing, is the surface tenseness of H₂O, is the denseness of H₂O, is gravitative acceleration, is the radius of the tubing and is the contact angle of the surface tenseness.

The old equation can be written in the undermentioned signifier: Where: is the radius of curvature.

Matric suction

The matric suction is the difference between the pore air force per unit area and pore H₂O force per unit area moving on the interface between air and H₂O (the contractile tegument) , this parametric quantity is associated to capillary tenseness in the pore H₂O (Fredlund and Rahardjo, 1993) . By taking the influence of matric suction in to account, the belongings of unsaturated dirt could be better interpreted (Fredlund 2000) . Entire suction is equal to: Where: s_m is the matric suction. u_a is pore air force per unit area and u_w is pore H₂O force per unit area. u_o is osmotic suction.

The osmotic suction is related to concentration of the dissolved salts in the pore H₂O. Osmotic suction is really of import for cognizing dirt belongings. However, the consequence of osmotic suction is normally neglected.

Therefore, the alteration in entire suction is equal to the alteration in matric suction (Fredlund 1989, Fredlund 1991) . Osmotic force per unit area can be measured by utilizing thermodynamic rules. Because of the osmotic suction is map of ionic concentration, the saturated and unsaturated dirt can be presented by utilizing this suction (Robinson and Stokes 1968) .

All surveies have shown that osmotic suction can hold an influence on the mechanical behavior of active clay stuffs. This influence of osmotic suction is related change of effectual emphasiss (Graham et al. 1988, Barbour and Fredlund 1989) . There are two chief factors which control the alteration of matric suction in clays, the factors are surface assimilation and capillary action (Richards 1974) .

The relation between matric suction and surface tenseness

The 4th stage on the unsaturated dirt which is the contractile tegument is supposed to have a surface tenseness which is related to the forces among the inter-molecular. Therefore, the contractile tegument will act as an elastic membrane as it is shown in the figure (2) . This behavior is similar to a balloon inflated with air which is the force per unit area inside this balloon is greater than the force per unit area outside it.

Because of the difference between the air force per unit area and H₂O force per unit area (matric suction) the contractile tegument takes the curve form. The undermentioned equation is Kelvin ' s capillary equation: From this equation it can be clearly seen that when the matric suction increases the radius of contractile tegument will cut down and the radius of contractile tegument will go to eternity when the matric suction is equal to zero.

The relation between the grade of Saturation and pore H₂O Pressure and in Unsaturated Soil

Nothingness in the unsaturated dirt can be filled with H₂O or air (water-filled or air-filled) .

These nothingnesss can be considered as a tubing which has radius (R) . Therefore, the matric suction will be equal to: Where: s is the matric suction and σ is the surface tenseness in the tubing as it is shown in the undermentioned figure: From the above equation it is clear that the matric suction is relative to the surface tenseness and reciprocally relative to the radius of the tubing. The nothingnesss in an unsaturated dirt it is non usually

to be filled partly with H₂O and filled partly with air. Therefore, the nothingness will be filled with H₂O or air (Sharma 1998) .

Suction measuring

it is really of import to mensurate and command suction in laboratory trial in order to understand the mecanical behavior of unsaturated dirts.

Suction is considered one of the two factors that control the behaviour of unsaturated dirts (Fredlund et Al, 1994 ; Lu and Likos, 2004) . The job of unsaturated dirt is that the pore H₂O force per unit area is negative with regard to atmospheric force per unit area. Achieving the same status in the research lab will bring forth so cavitation phonmona which is the creative activity of bubble in H₂O force per unit area these bubbles will do an erro of using and mensurating the force per unit area.

In add-on, the measuring of the volume of H₂O will be wrong due to these bubbles. There are some methods have been made to better the suction measuring.

Axis interlingual rendition technique

The rule of axis interlingual rendition technique is that addition pore H₂O force per unit area, pore air force per unit area and entire force per unit area by equal sums. Therefore, the cavitations phenomenon will be prevented because pore H₂O force per unit area will go positive force per unit area Hilf (1956) . As it is shown in the figure (1) the entire emphasis will be increased from which is the entire emphasis in the research lab to which is the entire emphasis in the field, the pore air force per unit area will be

increased from (pore air force per unit area in the research lab) to (concentrate air force per unit area in the field) and the pore H₂O force per unit area will be increased from (the negative pore H₂O force per unit area in the research lab) to (the positive pore H₂O force per unit area in the field) . Therefore, the net emphasis (and the matric suction (will non be changed. One the other manus, the bar of the cavitations is considered as disadvantage of this technique because the cavitations phenomena in the field have a effect axis which will non be included in the research lab by utilizing interlingual rendition technique.

The demand of axis interlingual rendition is accomplishing continuity of air infinite in the specimen this can be achieved by utilizing saturated high air entry such as ceramic disc which will do isolation between H₂O and air in the dirt because this disc will let the entryway of H₂O and forestall the entryway air. In add-on, this effektivance of this technique requires the grade of impregnation less 70 % . Bocking and Fredlund (1980) .

Osmotic control of matric suction

The rule of osmotic control of matric suction is based on the construct of osmosis. For illustration, semi-permeable membranes locate between the sample of dirt and osmotic solution such as molecules of polythene ethanediol. The membrane is porous to ions in the dirt and H₂O.

However, the membrane is impermeable to big solute molecules and dirt atoms (Zur, 1966) . The most of import advantage of utilizing the osmotic control for matric suction is that the cavitation due to the negative pore H₂O force per unit area is allowed to occure as the existing field status.

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furthermore, there is no demand to raise the cell force per unit area as in the axis interlingual rendition technique to make a high (Delage et al. 1998) . On the other hand the osmotic control technique has some disadvantages.

One of these disadvantages is that the trouble of accomplishing uninterrupted fluctuation of suction, due to the variation of the polythene ethanediol concentration. The 2nd drawback is the semi-permeable membrane is really weak if it is subjected to inordinate emphasis (Delage and Cui, 2008) .

Effective emphasis

Effective emphasis (l^*) it is a indispensable province variable to depict the province of emphasis within the dirt (Fredlund and Rahardjo, 1993) . Therzaghi (1943) used the emphasis province variable to command the dirt behavior and considered the effectual emphasis moving on saturated dirt are the difference between the entire emphasis, and the pore H₂O force per unit area.

Where: l^* is the effectual emphasis, l is the entire emphasis and u is the pore H₂O force per unit area. The theory of the effectual emphasis expressed that the distortion behavior of the dirt is controlled by effectual emphasis. However, for unsaturated dirt there are two extra parametric quantity must be considered (1) the pore air force per unit area (u_a) , which is the emphasis within the air stage and (2) the matric suction (l^*) , which is the difference between the pore air force per unit area (u_a) and the pore H₂O force per unit area (u_w) , (Lu and Likos, 2004) .

(Fredlund and Rahardjo, 1993) stated that Bishop (1959) has modified Terzaghi ' s effectual emphasis theory to explicate the effectual emphasis in unsaturated dirt as it is shown in the undermentioned equation: Where: u is the effectual emphasis, u_a is the pore air force per unit area, u_w is the entire emphasis, and u_w is the pore H₂O force per unit area, e is the effectual emphasis parametric quantity which is related to the grade of impregnation of the soil. The value of the effectual emphasis parametric quantity for concentrated dirt is equal to one unit and it is equal to zero for dry dirt. Aitchison (1961) expressed the relationships between the matric suction and the effectual emphasis factors in the undermentioned equation: Where: α is parameter which his value between from 0 to 1 and u_w is the force per unit area lack, Jennings (1961) , used the undermentioned equation to show the effectual emphasis for an unsaturated dirt: Where: α is parametric quantity which his value between from 0 to 1 and u_w is pore H₂O force per unit area which is taken as positive value. Richards (1966) , added the solute suction factor into the effectual emphasis equation: Where: u is effectual emphasis parametric quantity for matric suction, u_m is matric suction, u_s is effectual emphasis parametric quantity for solute suction, and u_s is solute suction.

Aitchison (1973) , proposed the undermentioned equation for the effectual emphasis of unsaturated dirt which is similar to Richards equation: Where: u is matric suction, u_s is solute suction, and α and β are soil parametric quantity which have value between 0 to 1 depend on the stress way. All old equation of effectual emphasis for unsaturated dirt based on incorporated the dirt parametric quantity by utilizing a individual value of effectual emphasis. The magnitudes of the dirt parametric quantity is different for different types of

dirt, different emphasis waies and different jobs such as volume alteration versus shear strength (Jennings and Burland, 1962 ; Coleman, 1962 ; Bishop and Blight, 1963) . Research workers suggested to utilize two independent emphasis province variables to depict the mechanical behavior of unsaturated dirts after they examined the proposed effectual emphasis equations because the usage of independent emphasis province variables has resulted in more meaningful account of unsaturated dirt behavior. (Bishop and Blight, 1963 ; Matyas and Radhakrishna, 1968) .

When dirt are subjected to a shear emphasiss and normal, the strength of the dirt increases up to a point where it can no longer defy shear emphasiss. Terzaghi (1936) used effectual emphasis variable in Mohar-Coulomb theory to foretell the shear strength of saturated dirts. The equation of the shear strength of concentrated dirt is additive map as follow: Whereis the shear strength. is the effectual coherence. is the effectual angle of internal clash. is the entire normal emphasis on the plane of failure. is the pore H2O force per unit area.

is the effectual normal emphasis on the plane of failure. However for unsaturated dirt the shear strength can be illustrated by utilizing any two of these three emphasis province variables: , and by (Fredlund and Morgenstern, 1977) . The undermentioned equation for shear strength of unsaturated dirt has been proposed by (Fredlund et al 1978) . Whereis the angle which point out the rise of shear strength with regard to a alteration in matric suction when and are used as two province variables.

is the angle which point out the rise of shear strength with regard to a alteration in matric suction when and are used as two province variables. The above equation shows a additive relationship between matric suction and shear strength. However, there were surveies have shown that the additions of shear strength in unsaturated dirts is non additive with an addition in matric suction. the account of these different consequences is that, at the beginning, the shear strength additions linearly with the addition of matric suction up to value above this value the additions of strength turn out to be non-linear. Moreover, the strength is tend to be changeless or bead down with high matric suction (Fredlund and Rahardjo 1993) . Lamborn (1986) presented a shear strength equation for unsaturated dirts as follows: Where is the volumetric H₂O content which is equal to ratio of the volume of H₂O to the entire volume of the dirt. The volumetric H₂O content reduces as matric suction rises. Peterson (1988) expressed the shear strength for dirt that has a grade of impregnation less than 85 % in the undermentioned equation: Where: is the coherence because of the suction.

The consequence of dirt suction on shear strength in the above equation is considered as rise in the coherence of the dirt. The coherence due to suction is reliant on the H₂O content of the dirt.

Volume alteration

The analysis of emphasis theory for an unsaturated dirt expressed that the independent emphasis variable, , and can be used to depict the volume alteration behavior and the shear strength behavior of an unsaturated dirt (Fredlund and Morgenstern 1977) . The volume alteration is one of the most

unsafe characteristics of the dirt which affect the substructure. The volume of unsaturated dirt either addition or lessening when it is subjected to wetting, this behavior is due to the using emphasis degree (Gens, 1996) . Because of the fact that the nothingness between atoms in concentrated dirt are filled with H₂O. Therefore, the volume alteration of a saturated can be measured by calculate the flow of H₂O coming in or coming out of the sample (presuming the volume of the solid dirt is changeless) .

However, the volume alteration of unsaturated can non be measured by the same manner because the nothingness between the atoms are filled with air and H₂O. Therefore, in order to cognizing the volume alterations of unsaturated dirt based on mensurating the volume alteration of the stages of unsaturated dirt. The cardinal points about the measurment of volume alteration in unsaturated dirt by utilizing triaxial trial is summrised in the undermentioned points by (Sharma, et Al. (2006)) : 1.

in the triaxil trial for unsaturated dirt the measurment of volume alteration can non be achieved by montoring the H₂O flow or escape from the spicement. 2. the measurment of the volume alteration for unsaturated dirt depend on cognizing the volume of each stage of the dirt, the overall volume alteration of the speciment and kowing the alterations of H₂O volume in the speciment every bit good as presuming the volume of the solid dirt is changeless. 3. the volume of H₂O alterations in the spicement of unsaturated dirt is similar to the measurment for spicement of saturated dirt by mensurating the H₂O influx or H₂O outflow from the dirt speciment.

There are two effectual manner two step the volume alteration of

unsaturated which are internal local strain measurements and the inner cell technique (Cabarkapa and Cuccoillo, (2006)) : The principle of utilizing the inner cell technique for measuring the volume alteration of unsaturated dirt is depend on the measurement of the flow of H₂O coming in or coming out of the cell.

The advantage of utilizing this technique is that the values of overall volume alteration is really precise. On the other manus, utilizing the inner cell technique for measuring the volume alteration of unsaturated is considered to be really sensitive for any alteration in force per unit area and temprature (Sivakumar (1993) , Cabarkapa and Cuccoillo, (2006)) . The volume alteration of unsaturated dirt can be measured by utilizing internal local strain measurement which measures the overall volume alteration by measuring the strain in two way perpendicular and radial straight by putting instruments in these way to the dirt sample.

Therefore, this technique gives a really accurate values of the volume alteration of the sample. On the othe manus, internal local strain measurement has a drawback because this technqe can be valid for stiff specimens which does non stand for the natural dirt status in the field (Cabarkapa and Cuccoillo, (2006)) .

The alteration for Triaxil setup

The setup of the Triaxial trial is used to mensurate many parametric quantities of concentrated dirt such as the permeableness of dirt shear strength features, consolidation features. This setup has been modified to mensurate unsaturated dirt parametric quantities by commanding pore-

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water, pore-air force per unit areas and volume alterations. There are some alteration has been done on conventional Triaxial setup for unsaturated dirt which will let commanding both pore-air and pore-water stages of a trial sample, and therefore analyze the consequence of matric suction on the behavior unsaturated dirt. The matric suction will remain stable under undrained conditions for dirt holding a low grade of impregnation and subjected to a low emphasis.

It was agreed that by utilizing dirt with an initial grade of impregnation about 32 % , this will do the passage emphasis to be about 50 kPa. Wulfsohn et. Al. (1998) . The modern triaxial system can mensurate the coefficient of permeableness of a concentrated dirt with a coefficient of permeableness every bit low as 5×10^{-11} m/s. whereas, the measuring of coefficient of permeableness can be much lower than 5×10^{-11} m/s for unsaturated dirt. There is a little lessening in the coefficient of permeableness of the dirt with the addition of matric suction from (0) up to the air-entry. However, the coefficient of permeableness will worsen aggressively when the value matric suction surpass the air-entry value.

(Huang, (1996)) In the triaxial proving the volume alteration of a dirt sample in is an indispensable parametric quantity, which has to be calculated and it is really of import for understanding the volumetric compaction of the dirt. The volume alteration due to consolidation of concentrated sample in Triaxial testing is equal to the volume of H₂O coming out of the sample. As a consequence, the best manner to cipher the volume alteration is by mensurating the volume of H₂O coming out from the sample.

Whereas, the volume alteration due to consolidation of unsaturated sample in Triaxial testing is non equal to the volume of H₂O coming out of the sample. Therefore, utilizing the volume of H₂O coming out from the sample to mensurate the volume alteration is non valid in unsaturated dirt. The first successful effort to mensurate the volume alteration was by Bishop and Donald (1961) . They put an unfastened inner cylindrical container in a conventional cell. The inner cell was filled with quicksilver and the infinite between the inner and outer cell was filled with H₂O and therefore the volume alterations of the unsaturated dirt sample can be measured by supervising the perpendicular motion of a steel ball which is drifting on the surface of the quicksilver.

Yin (1998) used the same thought of adding another cell to a conventional cell. The inner cell was filled with distilled H₂O to specific place and the infinite between the inner and outer cell was filled with air and therefore the volume alterations of the unsaturated dirt sample can be measured by supervising the perpendicular motion of the H₂O in the inner cell. However, this manner of mensurating the volume alteration in the dirt sample is non accuracy due to the utilizing of bare oculus for mentoring the alteration of H₂O place. Wheeler (1988) has developed Bishop and Donald (1961) by utilizing dual cell in the triaxial system for proving unsaturated dirts with big gas bubbles. a H₂O burette was used to mensurate the volume of the inner cell and a local proving ring was used to mensurate the perpendicular axial burden. By utilizing a stop between interior cell top shaft and the lading Piston the potency of escape can be minimized.

The consequence of support on the behavior of unsaturated dirt

The behavior of dirt with fiber support has been studied over the last two decades. Reinforcing the dirt with fiber is considered a feasible method for geotechnical technology jobs.

It was found that the shear strength of the dirt increases with the addition of fiber content in the sample. This addition of shear strength was relative to fiber content or content ratio (3, 5, 6, 7, and 8). But, over 8 the addition in the strength was non relative to the support concentration. In addition, the coherence and angle of internal friction in the dirt with fiber support will increase with the addition of fiber content. (Wei Chen, (2006)). Procedure
The first problem for covering with unsaturated dirt is the measuring of negative pore water force per unit area that because of water cavitations at a force per unit area more or less of -1 atmosphere.

There are some techniques that have been invented to get the better of the cavitations phenomenon such as axis interlingual rendition technique. The rule of axis interlingual rendition technique is increasing the ambient air force per unit area by a certain sum, and increasing the pore-water force per unit area by the same sum, that will maintain matric suction invariable (Hilf, 1956).

Samples readying

Wulfsohn et. Al. (1998) the samples can be undisturbed field samples or remoulded specimens prepared in the research lab. However, there is little

difference which is undisturbed samples present the field conditions better than remoulded samples.

The readying of remoulded samples is packing a dirt sample to specific H₂O content and denseness in a particular mold. [hypertext transfer protocol:](#)

[//www. soilvision. com/subdomains/unsaturatedsoil. com/Docs/Research % 20Papers/1998/Journal % 20Papers/Triaxial % 20testing % 20of % 20unsaturated % 20agricultural % 20soils. pdf](http://www.soilvision.com/subdomains/unsaturatedsoil.com/Docs/Research%20Papers/1998/Journal%20Papers/Triaxial%20testing%20of%20unsaturated%20agricultural%20soils.pdf)Aitchison, G. D.

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